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Impact of moisture content on instant catapult steam explosion pretreatment of sweet potato vine

Li-Yang Liu^{2,3}, Jin-Cheng Qin^{1,3}, Kai Li¹, Muhammad Aamer Mehmood^{1,4*} and Chen-Guang Liu^{1*} 

Abstract

Background: Lignocellulose originating from renewable and sustainable biomass is a promising alternative resource to produce biofuel. However, the complex component, especially high moisture content, leads to a higher cost of transportation and processing. The instant catapult steam explosion (ICSE) pretreatment can exploit the intracellular water of lignocellulosic materials and convert into vapors leading towards the breakdown of the feedstock during the explosion process. However, it is necessary to study the impact of moisture content on the pretreatment.

Results: The sugar yield of wet feedstock after ICSE pretreatment reached 88.05%, which was higher when compared to dried and untreated biomass. The utilization of wet feedstock decreased the production of inhibitor and improved the carbohydrate content in ICSE-treated biomass. There occurred a shrinkage of feedstock after drying process and the mechanical breakage upon ICSE pretreatment. Moreover, not all water was converted into vapor to cause breakage in the lignocellulose.

Conclusion: ICSE has shown to be preferably suitable to pretreat wet sweet potato vine with high moisture content, either fresh or soaked biomass that has been dried before. By using these materials, it would have a higher sugar yield and lower inhibitor production after pretreatment. Based on these advantaged aspects of ICSE platform, two potential strategies are proposed to improve the economic and environmental impacts of pretreatment.

Keywords: Pretreatment, Moisture content, Instant catapult steam explosion, Sweet potato vine, Enzymatic hydrolysis

Background

Nowadays, lignocellulosic biomass offers a promising alternative to produce biofuel owing to its abundance, renewability, and sustainability. However, the recalcitrant nature of biomass requires additional pretreatment steps to make it susceptible to cellulolytic enzymes (Mosier et al. 2005). Generally, pretreatment efficiency depends on low moisture content and small particle size of the biomass which also would reduce the cost of transportation (Vidal et al. 2011). However, traditional drying

process is an energy intensive process and the solar irradiance is limited in countries like China as compared to South Asia or Africa; thus, the air-drying process will occupy vast agriculture area preventing in-time crop rotation. So, to keep the crop rotation framework intact, most of lignocellulosic biomass is burnt on the field during harvesting seasons in northern China, causing atmosphere pollution and public health hazards (Tan et al. 2010; Qu et al. 2012). Alternatively, this low-cost biomass may be subjected to efficient pretreatment which do not involve drying step.

Fortunately, steam explosion pretreatment in principle requires higher moisture content in lignocellulose biomass, which may improve the efficiency of pretreatment. The biomass is usually treated under high pressure for several seconds to minutes to prompt the hydrolysis of

*Correspondence: draamer@gcuf.edu.pk; cg.liu@sjtu.edu.cn

¹ State Key Laboratory of Microbial Metabolism, School of Life Sciences and Biotechnology, Shanghai Jiao Tong University, Shanghai 200240, China ⁴ Department of Bioinformatics and Biotechnology, Government College University Faisalabad, Faisalabad 38000, Pakistan
Full list of author information is available at the end of the article

hemicellulose content and then release the pressure with a short time to break the microstructure of lignocellulose (Galbe and Zacchi 2012). Previous researchers adopted steam explosion to pretreat wet corn stalk and found that higher initial moisture content would improve enzymatic hydrolysis of lignocellulose and reduce 20% of steam consumption, because water in feedstock presented a buffering effect on reaction during steam explosion process (Sui and Chen 2015).

However, the traditional steam explosion instrument will produce abundant of inhibitors such as acetic acid, furfural, coumaric acid, and 5-hydroxymethylfurfural (5-HMF). Moreover, the longer pretreatment time will consume more energy (Cullis et al. 2004). To offset these drawbacks, instant Catapult Steam Explosion (ICSE) was invented. The short de-pressure time (0.0825 s) and pretreatment duration (1–5 min) provide ICSE huge mechanical force to destruct the biomass structure and less energy consumption with simple operation than traditional steam explosion (Gong et al. 2012). Previously, it has been demonstrated that ICSE can improve the enzymatic degradability of lignocellulose with few inhibitors and less energy consumption (Liu et al. 2014a). ICSE also has positive impacts on the efficiency of subsequent chemical pretreatments involved with organic solvent, acid, and alkali (Liu et al. 2014b).

Sweet potato (*Ipomoea batatas*) belongs to the family *Convolvulaceae*, containing abundant starch in the root. So far, China being the largest producer of sweet potato in the world has planted over 6.2 million hectares, and produces over 71 million tons of sweet potatoes, which accounts for the 67% of the global production (Fao 2016). The high sugar content and easily cultivated in saline and alkali land of sweet potato allow it to be used as an excellent resource to produce biofuels (Xia et al. 2013). Although significant advancements have been made on the conversion of sweet potato yet the progress made is not up to the desired levels. Many sweet potato vines including leaves, stems, and petiole are disposed in the farming field or used as low-value product like animal feed (Tian et al. 2009). Comparing with other lignocellulose resources such as corn stover and rice stalk, sweet potato vine contains higher moisture content and extractives (Jibril et al. 1999). These characters may be helpful to study the effects of lignocellulosic moisture content on ICSE pretreatment.

In present study, sweet potato vines were used to study the effects of moisture content on ICSE pretreatment by investigating the composition, inhibitors production, sugar yield, and thermal stability, for different feedstock including fresh feedstock, naturally dried feedstock, manually dried feedstock, and soaked dried feedstock. It was studied as a simple and practical method to obtain wet lignocellulose for both industry and lab.

Methods

Biomass collection and management

Fresh sweet potato vines were collected from a field near the city of Dalian in China during the summer, which contained 16.8% cellulose, 9.6% hemicellulose, 42.89% lignin and ash, 17.6% protein, and 1.5% fat after dried. Collected materials were cut into 1- to 2-cm fragments by scissors, and stored at -20°C for further use.

Fresh feedstocks (FF) were treated in different ways to obtain materials with different moisture contents. FF was dried by natural environment under the sun for 1 week (NDF), which was close to the natural condition before collecting the samples from the field. FF was also dried at 65°C to the constant weight. This manually dried feedstock (MDF) is widely accepted for the pretreatment.

Samples with coordinating water were also prepared by soaking 20 g MDF into 200 mL of tap water at room temperature at a short time for 2 h (SF-2), medium time (30 h, SF-30), and a long time (60 h, SF-60). To stop the soaking processing and stabilize the moisture content, the Buchner funnels with filter paper were used to separate the liquid and wet feedstock. Water on the surface of wet feedstock was cleaned by filter paper, following to put in the desiccator to stabilize their moisture content for 24 h. All feedstocks were sealed and stored at -20°C .

Chemicals and enzymes

Analytical grade glucose, xylose, furfural, 5-hydroxymethyl furfural (5-HMF), acetic acid, and coumaric acid were purchased from Sangon Biotech Corp. (Shanghai, China) and Solarbio Life Science Corp. (Beijing, China). Cellulase (GENENCOR accelerase 1500, cellulase enzyme activity: 105 FPU/mL) was kindly donated by Dupoint Genicor Science Corp. (Shanghai, China).

ICSE pretreatment

20 g of biomass including FF, NDF, MDF, SF-2, SF-30, and SF-60 were loaded directly into 400-mL chamber of the ICSE equipment (QBS-80B Steam Explosion Test Bed, Henan Hebei, Zhengdao Corp.). Steam with pressure (3.25 MPa) and temperature (240°C) was prepared in advance and sent into the chamber to make the pre-treated pressure be stabilized at 2.8 MPa for 90 s by controlling the quantity of flow. After this pretreatment, the ICSE-treated sweet potato vines were released from the chamber by depressurization in 0.0825 s, causing treated material to explode into a stainless-steel cyclone. The slurry (treated material) was collected by scoop into the plastic bag, and then sealed and stored at -20°C for further compositional and enzymatic hydrolysis analysis (Liu et al. 2014a).

Moisture content analysis

The moisture content (C_{m1}) of materials before and after ICSE pretreatment was calculated via the equation

$$C_{m1} = (X_1 - X_2)/X_1,$$

where X_1 is the mass before oven drying and X_2 is the mass after drying in the 65 °C oven to get a constant weigh.

Inhibitor and sugar analysis after ICSE pretreatment

5 grams of each of the ICSE-treated materials were centrifuged in 1957×*g* for 10 min. The supernatants were used for inhibitor and sugar concentration (C_i) analysis by high-performance liquid chromatography analysis. The solid components were dried at 65 °C to get a constant weight (X_3). After the analysis of liquor solution, the inhibitor and sugar yield (mg/g) after ICSE pretreatment were calculated by the equation: inhibitor yield = $C_i \times (5 - X_3)/X_3$. All experiments were performed in triplicate and the results are presented as mean and standard derivation.

Compositional analysis

Untreated MDF and solid components of ICSE-pretreated samples were totally dried and finely ground to less than 40-mesh. 100 mg of each sample was mixed with 1 mL of 72% (w/v) sulfuric acid, and placed in the 50-mL colorimetric tube. The tubes were incubated at 30 °C water bath for 1 h with stirring every 10 min to ensure the intensive mixing. After 1 h, final concentration of acid was brought to 4% by adding 28 mL of deionized water, and was put in the autoclave at 121 °C for 1 h. After that, all tubes were left to cool down to room temperature, and the treated samples were filtered by the Buchner funnel with Whatman No.1 filter paper. The supernatants of each tube were used to analyze the glucose, cellobiose, xylose, and arabinose, representing cellulose and hemicellulose, respectively. The solid components were thoroughly washed and dried until it reached a constant weight, representing lignin and ash content. All experiments were performed in triplicate and the results are presented as mean and standard deviations (Sluiter et al. 2012).

Enzymatic hydrolysis

Untreated and the solid fractions of ICSE-pretreated samples were accurately weighted (300 mg) and placed in the 50-mL colorimetric tubes, suspended in 30 mL buffer solution (acetic acid, pH 4.8) containing the enzyme at the ratio of 30 FPU/g. The mixture was incubated at 50 °C for 48 h followed by a centrifugation. Supernatant was subjected to sugar content analysis, as described

previously (Liu et al. 2014a, b). The sugar yield was calculated by Eq. (1) below:

$$\text{Sugar yield(\%)} = \frac{[(\text{glucose} \times 0.9) + (\text{xylose} \times 0.8)]}{\text{carbohydrate in biomass}} \times 100. \quad (1)$$

Glucose and xylose were analyzed by the HPLC. All experiments were performed in triplicate, and results are presented as mean and standard deviations.

High-performance liquid chromatography analysis

The supernatant from ICSE-pretreated samples and enzymatic hydrolysis were filtered through 0.45- μ m filter and 20 μ L of each sample was loaded to the ion exclusion column (300 mm \times 7.8 mm, Bio-Rad, Hercules, Aminex HPX-87H) at 50 °C in HPLC system equipped with a refractive index detector and UV detector (Waters, MA, USA), for the quantitation of inhibitors and saccharides. Sulfuric acid 0.01 mol/L was used as mobile phase at flow rate 0.5 mL/min (Liu et al. 2014a).

Scanning electron microscopy (SEM)

The microscopic morphology changes in the untreated and ICSE-pretreated samples after dried by lyophilization were observed using SEM. Each of the samples was placed on the aluminum sample platform and scanned by environmental scanning electron microscopy (Quanta 450, FEI, USA 20 kV), using 20 kV as described previously (Liu et al. 2014a).

Thermal gravimetric analysis (TGA)

About 10 mg of freeze-dried MDF, ICSE-treated FF, and ICSE-treated MDF were placed in the platinum crucibles for thermal degradation analyses using TGA Q500 (TA Corporation, USA). Samples were heated from 25 to 500 °C at a constant heating rate of 10 °C/min under nitrogen atmosphere at the flow rate of 50 mL/min (Carrier et al. 2011).

Results and discussion

The change of moisture content in different feedstock

Moisture content of any plant biomass is an important parameter for its subsequent usage as a feedstock for bioenergy. To evaluate the effect of moisture content on pretreatment and enzymatic hydrolysis, five forms of samples were prepared (Table 1). FF normally contains 80.50% to sustain the growth of plants. NDF shown to contain 63.57% moisture content which was obtained through exposure of harvested FF under the sun for 7 days. MDF was subjected to soaking to regain the moisture content. Interestingly, the moisture content of SF immediately came up to 62.93% through submerging

Table 1 The moisture content and the compositional analyses of liquid phase after ICSE pretreatment

Feedstocks	FF	NDF	MDF	SF-2	SF-30	SF-60
Moisture content (%)						
Untreated	80.50	63.57	0.97	62.93	83.38	84.24
Pretreated	96.95	96.04	93.30	95.62	97.90	97.29
Liquid contents						
Pretreated (mg/g)						
Glucose	0.7865 (0.0649)	0.3798 (0.0123)	0.2638 (0.0279)	0.0284 (0.0091)	0.0008 (0.0012)	0.0000 (0.0000)
Xylose	0.8858 (0.0577)	0.5393 (0.0292)	0.4733 (0.0320)	0.0682 (0.0137)	0.0031 (0.0020)	0.0006 (0.0000)
Acetic acid	0.0768 (0.0049)	0.0926 (0.0007)	0.1293 (0.0019)	0.0496 (0.0015)	0.0674 (0.0517)	0.0000 (0.0000)
Coumaric acid	0.2405 (0.0827)	0.4769 (0.0303)	0.7838 (0.0149)	0.2797 (0.0136)	0.0659 (0.1110)	0.0241 (0.0000)
5-HMF	0.0702 (0.0247)	0.0492 (0.0325)	0.0418 (0.0021)	0.0231 (0.0080)	0.0059 (0.0040)	0.0041 (0.0008)
Furfural	24.17 (2.18)	17.41 (0.74)	34.81 (0.96)	18.76 (1.04)	5.37 (1.40)	5.42 (0.24)

Data were shown as "mean (standard deviation)"

MDF for 2 h and finally stabilized at around 84.24% at 60 h. The moisture content of SF-60 was close to that of FF, which may be attributed to water absorption by favorable hydrophilic component and the sponge-like structure of lignocellulose (Dhakal et al. 2007). In addition, it is worth mentioning that, to achieve the same available biomass, the weight of MDF was one-fifth of FF, so the drying process could significantly reduce the total weight of lignocellulose, which is very important for biomass transportation (Axelsson et al. 2012). Moreover, soaking is a convenient way to regain the water, if required, after the easy transportation of dried biomass to the biofuel industry.

ICSE-pretreated sample contained higher moisture content ranging from 93.30 to 97.90%, which was caused by the abundant liquefied water condensed from the steam and stored in the pores of feedstock after the explosion (Table 1). Since the initial moisture content of feedstock also affects the final moisture content, it is obvious to get similar trends of moisture content after pretreatment. However, the ICSE pretreatment demonstrated its capability to smooth the difference of moisture content among all samples, which nullify the impact of drying on ICSE.

Composition and inhibitors in pretreated feedstocks

The pretreatment with high temperature that can contribute to enhance the available sugars upon hydrolysis is preferred in the bioconversion of biomass to biofuels. However, under high-temperature pretreatment, the lignocellulose will be partially degraded to inhibitors such as organic acid, furfural, 5-HMF, which drastically hinder the efficiency of enzymatic hydrolysis and fermentation process (Jönsson et al. 2013). The 5-HMF, furfural, and coumaric acid, respectively, represent the cellulose, hemicelluloses, and lignin, and reflect the compositional

Table 2 The compositional analysis of untreated MDF and the solid contents after ICSE pretreated

	Cellulose/%	Hemicellulose/%	Lignin and ash/%
Untreated			
MDF	16.83 (1.86)	9.60 (1.20)	42.88 (0.67)
Pretreated			
FF	40.25 (1.62)	10.27 (0.13)	22.39 (0.52)
NDF	41.10 (2.18)	10.92 (0.90)	19.66 (2.91)
MDF	41.96 (4.66)	8.23 (1.40)	24.76 (1.86)
SF-2	42.28 (1.75)	10.95 (1.96)	23.88 (4.41)
SF-30	48.69 (1.35)	15.04 (0.92)	20.40 (1.85)
SF-60	48.38 (0.31)	15.95 (0.86)	21.28 (2.77)

Data were shown as "mean (standard deviation)"

change of untreated and pretreated biomass (Vander et al. 2014).

Table 2 shows that ICSE improved the cellulose content from 16.83% (untreated MDF) to 40.25–48.69% (ICSE treated), accompanied with the reduction of "lignin" from 42.88% (untreated MDF) to 19.66–24.76% (ICSE treated) and the change of hemicelluloses content from 9.60% (untreated MDF) to 8.23–15.95% (ICSE treated). The "lignin" content in the solid phase was higher than that of references' data, since the protein, fats, and extractives may mix with lignin to impact the acid insoluble lignin and the acid soluble lignin (Jibril et al. 1999). In spite of considerable degradation of hemicelluloses under high temperature, the removal of abundant organic extractives and proteins helped hemicelluloses maintain the content percentage and even better (Zhan et al. 2013; Rocha et al. 2012). This may also explain the significant reduction of "lignin" content in feedstocks after ICSE pretreatment, since extractives, fats, or proteins in detected "lignin" might easily to be hydrolyzed within higher temperature

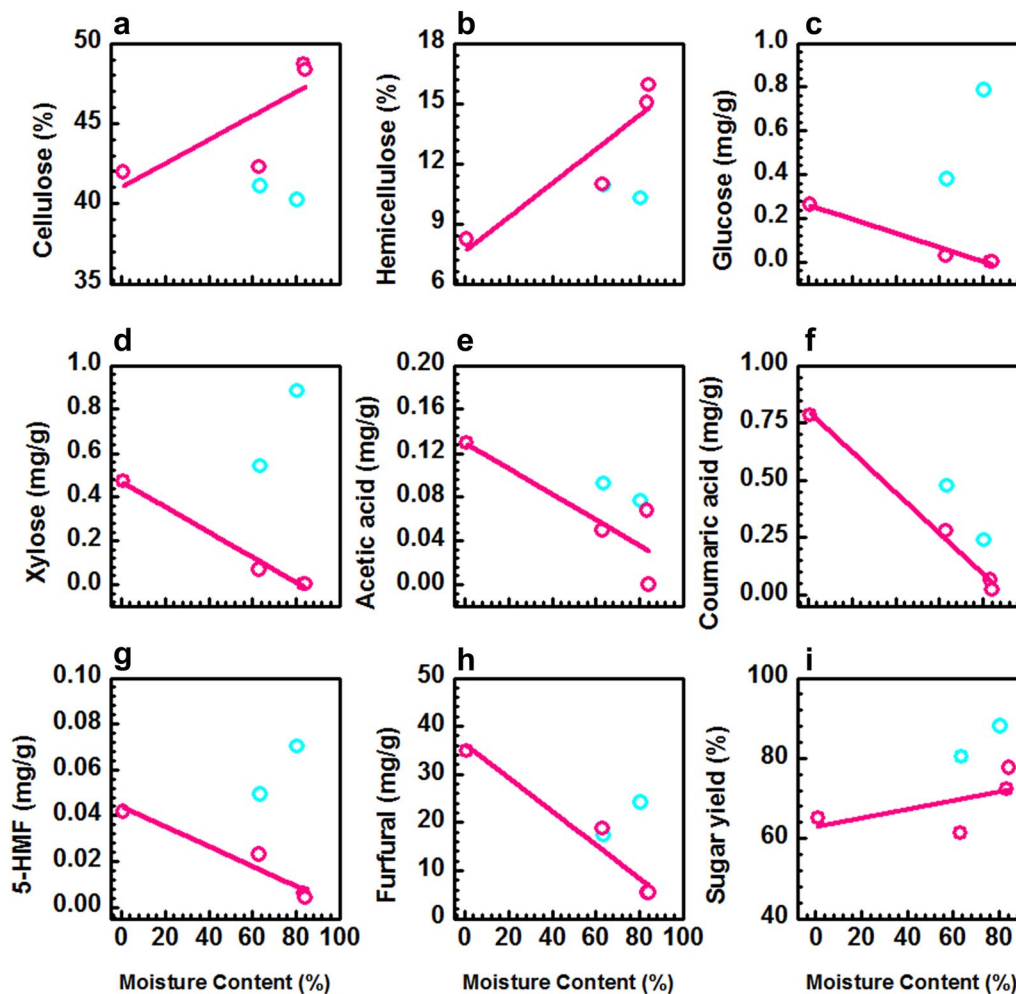


Fig. 1 Effects of moisture content on components, inhibitors, and sugar yield. Carbohydrates (**a** cellulose, **b** hemicellulose) in the solid fraction, sugar (**c** glucose, **d** xylose), and inhibitors (**e** acetic acid, **f** coumaric acid, **g** 5-HMF, **h** furfural) in the liquid fraction, and sugar yield (**i**) of ICSE-pretreated feedstocks after enzymatic hydrolysis. Cyan plots: FF and NDF; pink plots: MDF, SF-2, SF-30, SF-60

during ICSE pretreatment. Figure 1a, b shows the positive correlation for linear fitting between cellulose (hemicelluloses) and the moisture content in MDF, SF-2, SF-30, and SF-60 after ICSE pretreatment. Those four feedstocks marked in pink color share the oven-drying process in common. The oven-drying process with rapid dehydration of feedstock under higher temperature resulted in significant structure change from FF (Fig. 4). Therefore, it is worth noticing that two cyan scatters representing FF and NDF were non-compliance with the line correlation among those four feedstocks, since the plant's intracellular components would impact the yields of sugar and inhibitor at non-soaking conditions.

Figure 1c, d illustrates a negative correlation between glucose (xylose) in the liquid phase and the moisture content. The R^2 -value was more than 0.98 which strongly validates the reliability of linear relationships. Soaking

will dissolve low molecule sugar from feedstock, so the feedstock after long-time soaking lost a plenty of soluble sugar. Though the portion of glucose and xylose was derived from the thermal degradation of cellulose and hemicelluloses, ICSE mainly acts as physical pretreatment and produces little monosaccharides. Therefore, soaking is the prior factor to reduce the glucose and xylose in liquid phase. Interestingly, FF contained mostly glucose and xylose, which were nutrients for sweet potato cell in the vine after harvesting. After 7 days drying, the glucose and xylose decreased due to continuous respiration by living cells in NDF.

The inevitable high-temperature process during ICSE pretreatment converts some lignocellulose to inhibitory by-products such as 5-HME, furfural, acetic acid, and coumaric acid from hexose, pentose, and lignin, respectively (Table 1). The correlation of inhibitor and moisture

content was consistent with the relation between sugar and moisture content (Fig. 1). Among these inhibitors, the coumaric acid and furfural produced from lignin and hemicelluloses, respectively, were higher than others, which reflected that ICSE process could more easily hydrolyze lignin and hemicelluloses than cellulose (Liu et al. 2014a). Since soaking is analogous to washing and can rinse monosaccharides and oligosaccharides out of the material surface (Frederick et al. 2014), longer soaking time diminished the surface residual sugars and subsequently decreased the accumulation of inhibitors during ICSE pretreatment (Table 1).

The pretreatment efficiency is not only determined by the moisture content of feedstock, but also by the method of feedstock handling. Therefore, the structure of feedstock should be analyzed for further understanding of this process.

Thermal degradation analysis of untreated and ICSE-pretreated feedstocks

Thermal stability of the biomass is analyzed by using TGA, a widely adopted technique to determine the thermal degradation of plant biomass (Carrier et al. 2011; Sanchez-Silva et al. 2012). In general, the differential-TG (DTG) curves of lignocellulose biomass often show three main peaks: one reflects the evaporation of extractives or water at 100–200 °C, the others stand for degradation of cellulose and lignin at 300–350 and 300–500 °C, respectively. The DTG curve usually exhibits shoulders in the temperature range of 200–300 °C, corresponding to the hemicelluloses degradation. The relative intensities of each peak could be used to calculate the quantities of hemicelluloses, cellulose, and lignin present in the lignocellulose (Carrier et al. 2011).

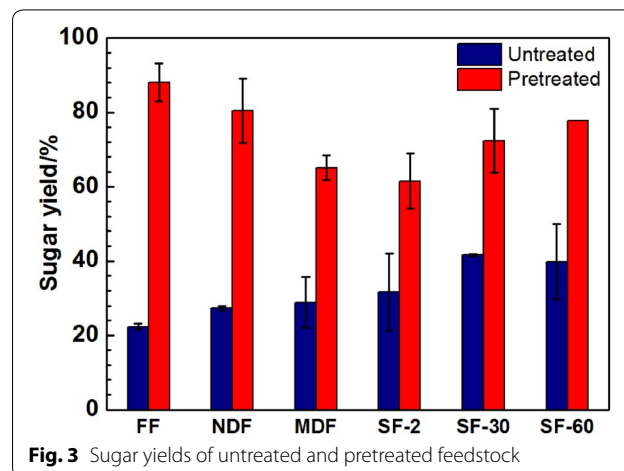
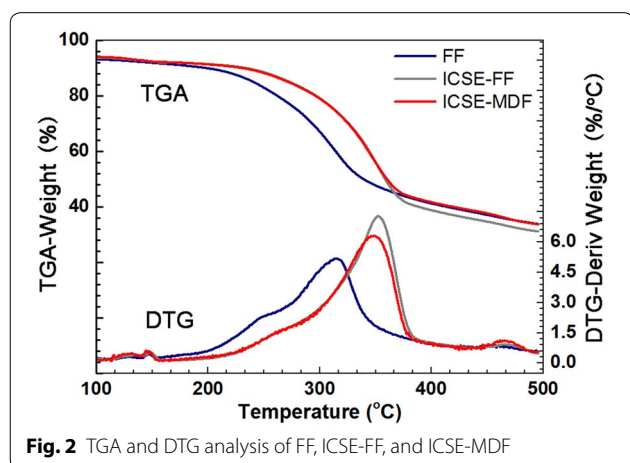
Interestingly, the respective hemicelluloses shoulder of MDF's DTG curve almost disappeared after ICSE pretreatment and the height of its maximum peak increased 12.5%

and moved to a higher temperature due to the degradation of hemicelluloses and the related lifting of cellulose (Fig. 2). Noticeably, it is highly consistent for the temperature and area of DTG curves' shoulder with a range from 200 to 350 °C between ICSE-FF and ICSE-MDF due to their minor variance of carbohydrate content, less than 0.66%. This finding was further confirmed by the compositional analysis (Table 2). In summary, ICSE pretreatment degraded the hemicelluloses content and nullified the impact of drying process on the change of lignocellulosic composition when compared to wet feedstock.

Impact of pretreatment on enzymatic hydrolysis

The enzymatic hydrolysis is the key step to obtain the fermentable sugars from lignocellulosic biomass. Before pretreatment, handling operation enhanced the structural and compositional change of feedstock (Table 2 and Fig. 3), which can be confirmed by sugar yield after enzymatic hydrolysis. NDF and MDF owned better sugar yield than FF, and soaking duration further improved the sugar yield. The soaking process could wash away some chemical composition that might inhibit enzymolysis or lead to invalid enzymatic adsorption (Frederick et al. 2014). In addition, the hornification effects due to the drying process for MDF might lead the plant to have a lower accessibility to enzyme or chemical reagents, which might also inhibit the enzymatic hydrolysis (Fernandes et al. 2004).

A considerable pretreatment method should ensure that pretreated feedstocks are suitable for robust saccharification (Agbor et al. 2011). Figure 1 illustrates that ICSE pretreatment significantly enhanced the enzyme hydrolysis when compared to the untreated feedstocks. Especially, the sugar yield of ICSE-FF was shown a fourfold increment and reached to the maximum value (88.05%) of all samples. At this condition, sugar concentration after enzymatic hydrolysis is about 5.18 g/L. Similar improvements were observed in NDF and soaked biomass. These



results indicate that higher moisture content is helpful to improve further enzymatic hydrolysis after ICSE pretreatment (Figs. 1i and 3); Sui and Chen drew the same conclusion by using normal steam explosion pretreatment on corn stover (Sui and Chen 2015). However, this impact was less obvious on the samples which were soaked for short durations, i.e., 2 h. In addition, whether it is treated or not, the sugar yield of SF-30 was close to SF-60. So, 30 h is enough to improve the degradability of lignocellulose. Though the moisture content of NDF and SF-2 was similar (about 63%), their sugar yields were quite different due to the hornification effect. Soaking process enabled lignocellulose to absorb moisture, but the shrinkage of internal fibers could not be fully recovered. It also demonstrated that the moisture content was not the only factor to predominate the enzymatic hydrolysis, but structure of feedstocks might be more pivotal on accessibility of cellulase than expected (Fernandes et al. 2004).

The morphological and micro-structural analysis on feedstock

So far, compared with MDF, ICSE pretreatment had more efficient impacts on FF and SF. The macroscopic appearance of feedstocks under different conditions is shown in Fig. 4; both FF and SF-60 were full of water, which seem to

be more resilient than dried feedstock. Similar with wood industry, the morphological structure of dried wood could get back in shape after absorbing some water (Wang et al. 2006). Feedstock was destructed by steam explosion which turned into more uniform and reduced the particle size. As an order of destruction, FF occupied first place followed by dried feedstocks. It was interesting to note that soaked feedstock produced non-uniform particles when subjected to ICSE and some of the biomass components were unable to be reached by hot steam. The similar findings were observed previously, because the hornification effects would lead to different biomass structures between FF and SF and potentially impact ICSE pretreatment (Fernandes et al. 2004). Soaking could not infiltrate to all parts due to mass transfer limitation at short time, which formed the un-soaked tissue mainly located in inner part of biomass (Borrega and Kärenlampi 2010).

The sample used for SEM micrographs was dried by freeze-drying that preserved cell structure (Fig. 4), whereas the NDF and MDF undergone a drying process at ambient and moderately high temperature, and their cell wall becomes very vulnerable due to dehydration. As shown in Fig. 4, the pores in FF were biggest among three feedstocks, which facilitate the steam or hot water penetrating biomass and enhancing explosion force to

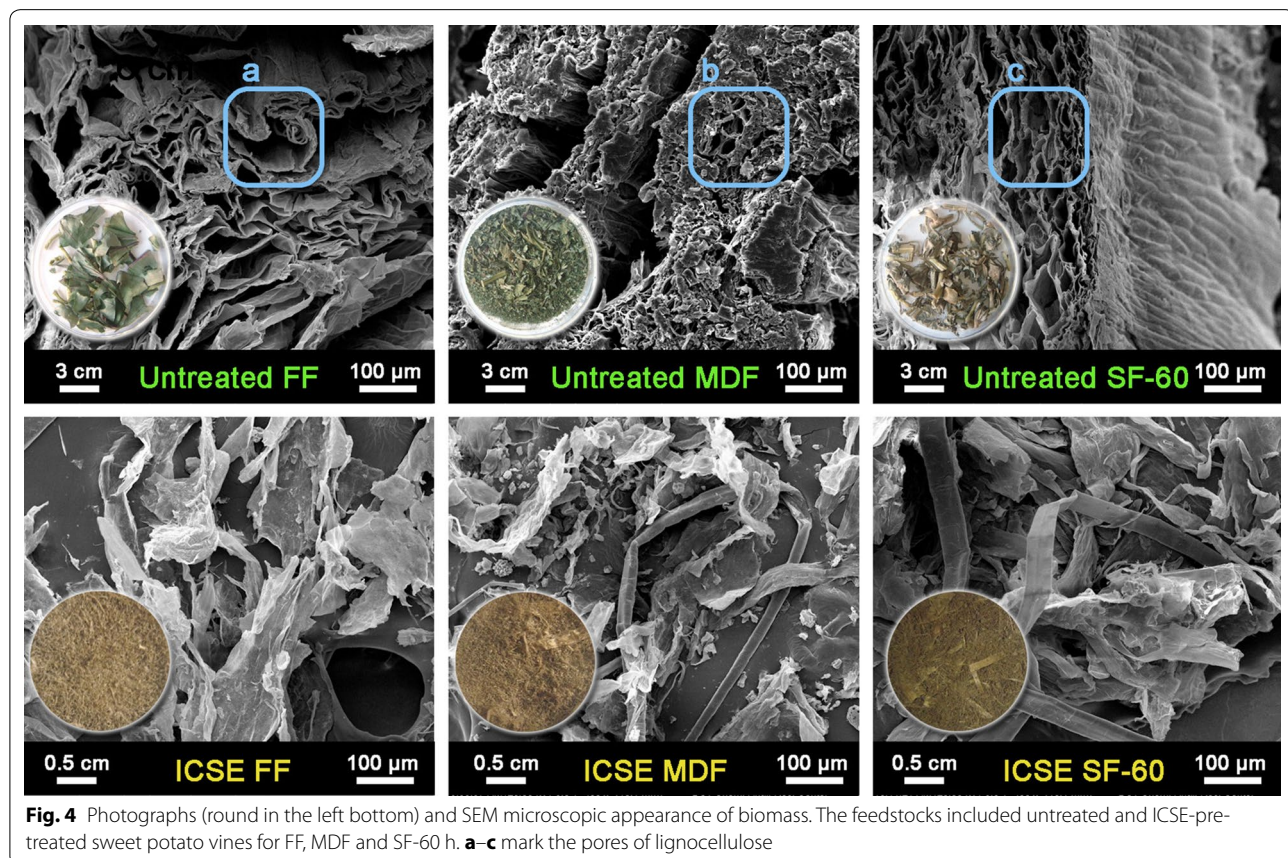


Fig. 4 Photographs (round in the left bottom) and SEM microscopic appearance of biomass. The feedstocks included untreated and ICSE-pretreated sweet potato vines for FF, MDF and SF-60 h. **a–c** mark the pores of lignocellulose

degrade components. When the feedstock was totally dried, all pores in MDF shrank to about one twenty of area of pores in FF due the hornification effects (Fernandes et al. 2004). It blocked the entrance of steam and hot water into pores and lead to a lower accessibility of vapors. If the MDF was soaked in the water, the rehydrating feedstocks tend to return previous status with big pores. Nevertheless, the irreversible ruins on cell wall by drying process have occurred, which leads to the pores of SF much bigger than MDF's, but still smaller than FF's.

After ICSE pretreatment, all feedstocks were similar because of their similar moisture content (Table 1), but there was still obvious different observations by naked eyes. The particles of ICSE-pretreated FF were the smallest and distributed evenly. Inversely, the particles of ICSE-pretreated MDF were not homogeneous and the particle size was bigger than ICSE-pretreated FF particles. Some big debris could be found in pretreated MDF and SF-60.

The role of water and steam in ICSE pretreatment

Given the basic principle of steam explosion, the mechanical force is generated by the expanding gas (water vapors). So, changes of gas volume during the working temperature range may be helpful to enhance the destruction impact of the steam explosion. For

$$m_s = \frac{1 \text{ kg} \times (230 - 25)\text{K} \times (1.7 \text{ kJ/kg} \cdot \text{K} \times (1 - C_m) + 4.37 \text{ kJ/kg} \cdot \text{K} \times C_m)}{1812.6 \text{ kJ/kg}} \quad (4)$$

convenient evaluation, if pressure changes are ignored, 1 L air at 25 °C would be 1.7 L at 230 °C (Eq. 2). However, 1 L water at 25 °C would be transformed to 2100 L steam at 230 °C (Eq. 3). Therefore, higher moisture content potentially produces more inner steam for mechanical work which subsequently can destroy the compact structure of biomass. But the steam which is out of feedstock only can convert their thermal energy to kinetic energy.

$$\text{Air volume} = \frac{T_2 P_1}{T_1 P_2} V_1 = \frac{(230 + 273)\text{K}}{(25 + 273)\text{K}} \times 1\text{L} = 1.7\text{L} \quad (2)$$

$$\text{Steam volume} = \frac{1000\text{g}}{\frac{18\text{g}}{\text{mol}}} \times 37.8 \frac{\text{L}}{\text{mol}} = 2100\text{L} \quad (3)$$

In the small pores of biomass, the steam explosion process followed two steps. The first part is heating: the gas and liquid were heated from room temperature to setting temperature about 230 °C. The water in the biomass remained as liquid phase because the working pressure was always higher than saturated vapor pressure. So, the liquid hot water dissolved partial lignocelluloses and other water-soluble components. The next step was flash depressurizing. When the pressure in working vessel is instantly released to atmosphere pressure,

the vaporization from hot water generated huge volume steam subsequently causing biomass degradation.

Though the presence of higher moisture content seems attractive for steam explosion, however, the high moisture content of biomass would require more energy due to higher specific heat capacity of water. On the other hand, it would not possible for all liquid water to transform into steam during the explosion if the moisture content is high, even with heavier inputs of energy. Roughly calculation for the energy input and steam generation during steam explosion can be undertaken as Eq. 4, which showed the climbing amount of steam (m_s) with the increase of C_m , where, 1 kg biomass with C_m moisture content was heated from 25 to 230 °C (1.8 MPa). Since the change of specific heat capacity is little within this temperature range, the average values of specific heat capacity for water and feedstock are 4.37 and 1.7 kJ/(kg K), respectively. The vaporization heat of water at 230 °C is 1812.6 kJ/kg. When the C_m is lower than 27.50%, theoretically, the biomass should become completely dry subjected to ICSE. But what happened, the condensed water from heating steam increased the moisture content of pretreated biomass. Therefore, the moisture content of wet feedstock helped to remove the hemicelluloses and other water-soluble components, and generated more inner steam for improved explosion impact (Sui and Chen 2015).

Effects of moisture content on lignocellulose pretreatment

Due to the high moisture content of lignocellulose, researchers had studied its effects on various pretreatment methods such as ionic liquid pretreatment, grinding, and steam explosion (Table 3). Grinding of wet lignocellulose would consume more energy and finally have a bigger particle size than dried feedstock (Barakat et al. 2015). Mixing water with ionic liquid would lead to a lower pretreatment efficiency, though it would reduce reagents and the whole pretreatment cost (Shi et al. 2014a).

Fortunately, the moisture content of lignocellulose would improve pretreated efficiency of steam explosion or supercritical CO₂ pretreatment. Compared with dried feedstock, wet lignocellulose would prohibit the pyrolysis of hemicelluloses and facilitates the following enzymatic hydrolysis during steam explosion pretreatment (Sui and Chen 2015). In addition, previous works about some special steam explosion, such as the pre-soaking lignocellulosic biomass with SO₂ before the pretreatment (Cullis et al. 2004) and the addition of ammonia in the steam water (Moniruzzaman et al. 1997), showed higher sugar yield than ones obtained from dried feedstock and in agreement with this study. Considering the high cost of lignocellulosic pretreatment, the steam

explosion is a better option. It has an appealing trait, which does not require too much refining operation before pretreatment and allows simplifying the handling on raw feedstock.

Though researchers studied moisture effects on pretreatment efficiency, few of them studied impacts of intracellular moisture. Here, FF showed 88.05% sugar yield after ICSE pretreatment which was competitive when compared to other resources and steam explosion pretreatment. Conclusively, the sweet potato vines and ICSE would be an excellent resource and pretreatment process for the preparation of high-value substrates for microbial fermentation.

The strategies for feedstock collection and transportation

The collection, storage, transportation, and pretreatment of biomass are energy consuming processes. The moisture content has significant impacts on these processes (Kudakasseril et al. 2013). In US, cellulosic ethanol plant uses common feedstock like agriculture residue, which are naturally dried for 1–2 months in the fields and bunched by rotary baler. The dry feedstock could save the cost of transportation (Axelsson et al. 2012). However, this path is not suitable for cellulosic plants in China, because the agricultural residues cannot be allowed to stay too long in the field due to the following farming, and the wet feedstock with high moisture content is heavy enough to cost high transportation charges (Shi et al. 2014b).

The research has demonstrated that the fresh and soaked biomass (pre-dried) performed better after ICSE

pretreatment than dried feedstock, considering the dramatical improvement of carbohydrate content and sugar yield, and the lower production of inhibitors. Therefore, two strategies based on ICSE pretreatment were proposed (Fig. 5) for agricultural countries which are forced to use high-density cultivation such as China and Pakistan to fulfill the requirements of their huge populations.

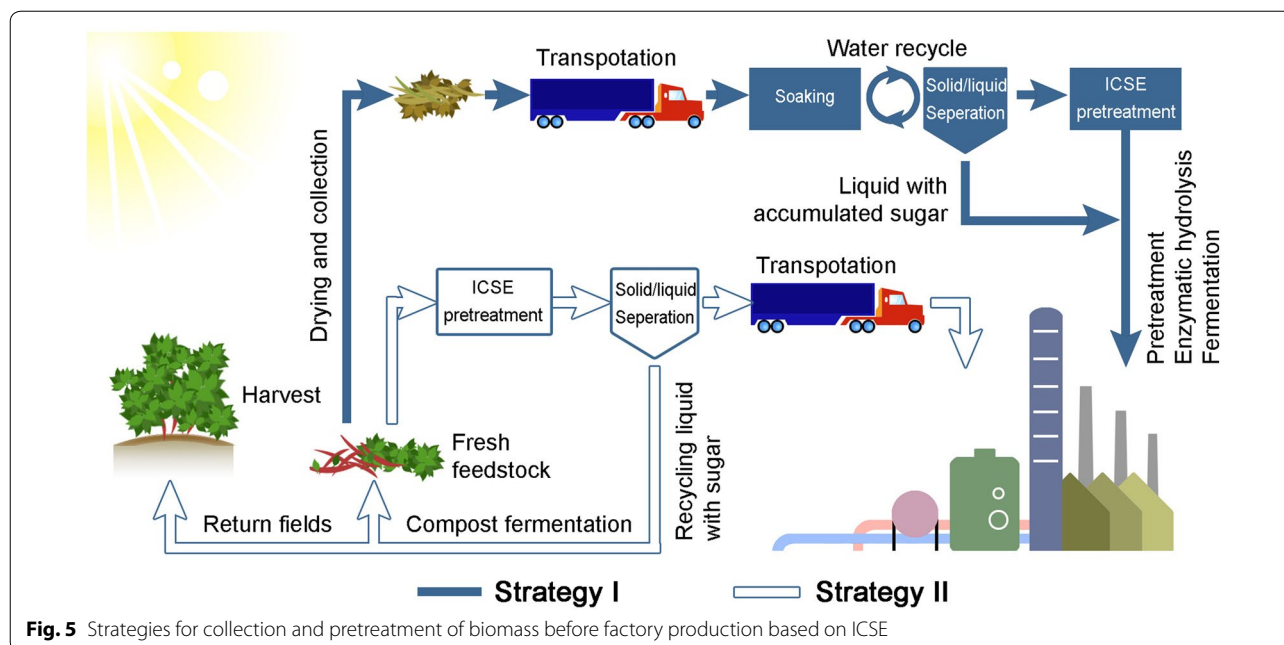
The first strategy follows the ordinary handling process before pretreatment, but the dry biomass needs to be soaked to regain the moisture content and to wash out the monosaccharides. The high moisture content will benefit the ICSE performance with the improvement of sugar yield. Attractively the soaked water can also be recycled for next soaking, which concentrates the soluble sugar form raw biomass and avoid the accumulation of inhibitors during thermal pretreatment.

In the second proposed strategy, fresh biomass may be directly subjected to ICSE at an adjacent working station near the farm. The liquid phase of pretreated biomass can be either returned to field as fertilizer or utilized for biogas production, since it contains plentiful organic compounds. The second strategy is more suitable to the populous countries, including China, where crop rotation is required either due to seasonal issues or due to heavy requirements of food and feed. For example, in eastern China, the crop residue should be moved quickly within 1 month for the following cultivation; thus, there is no time available for field drying (Rasmussen et al. 1980). Moreover, ICSE can efficiently decrease particle size by destroying the compact structure and elevate the sugar content, when fresh biomass is used. Moreover,

Table 3 Summary for the effects of moisture content on lignocellulose pretreatment

Pretreatment	Biomass	Sugar yield	Advantage	Disadvantage	Refs.
Ionic liquid	Switchgrass	70%	Decrease the cost of ionic liquid pretreatment	The existence of water will hamper the efficiency of pretreatment	Shi et al. (2014a)
Grinding	Wheat straw, corn stover etc.	NA	NA	Result in additional energy requirement and higher final particle size	Barakat et al. (2015)
Supercritical CO ₂	Southern yellow pine	84.7%	The increase of initial moisture content will obtain higher final sugar yield	NA	Kim and Hong (2001)
Steam explosion	Corn stover	90%	Improve the sugar yield	Not benefit for the quickly heating of biomass during pretreatment	Sui and Chen (2015)
Ammonia fiber steam explosion	Corn stalk	80%	Increase of moisture content does not hamper the enzymatic hydrolysis of lignocellulose	Ditto	Moniruzzaman et al. (1997)
Steam explosion	Softwood	60–90%	Prompt the enzymatic hydrolysis and reduce the hydrolysis of hemicelluloses content	Ditto	Cullis et al. (2004)
Acid steam explosion	Corn stover	> 90% (Xylose)	High soluble sugar yield	Ditto	Emmel et al. (2003)

NA not available



transportation of the onsite ICSE-pretreated solid to the biofuel producing plant can also save the time and cost, comparing with onsite drying or transporting fresh biomass (Fig. 5).

Conclusion

The present study focused on developing a low-cost strategy for the pretreatment of feedstock to biofuel-producing industry. The moisture content of lignocellulosic biomass can be utilized to enhance the enzymatic hydrolysis via ICSE, instead of drying. Moreover, ICSE pretreatment raises the carbohydrate content up to 1.43-folds with concomitant lowering of the inhibitors in the hydrolysate. The sugar yield of ICSE-pretreated fresh feedstock was improved by 2.5-folds and reached to 88.05%, which was like soaking the biomass for 60 h, suggesting that the use of fresh biomass would be the best way to run ICSE.

Abbreviations

ICSE: instant catapult steam explosion; FF: fresh feedstock; NDF: naturally dried feedstock; MDF: manually dried feedstock in oven; SF-2: soaking feedstock for 2 h; SF-30: soaking feedstock for 30 h; SF-60: soaking feedstock for 60 h; SEM: scanning electron microscopy; TGA: thermal gravimetric analysis; DTG: differential thermal gravimetric analysis; 5-HMF: 5-hydroxymethyl furfural.

Authors' contributions

LL carried out this experiment, data collection, data analysis, and manuscript preparation. CL conducted the research, investigation process, artwork, and manuscript preparation. JQ and KL made equal contribution to prepare initial manuscript. MAM revised the manuscript to its final form. All authors read and approved the final manuscript.

Author details

¹ State Key Laboratory of Microbial Metabolism, School of Life Sciences and Biotechnology, Shanghai Jiao Tong University, Shanghai 200240, China.

² Department of Wood Science, University of British Columbia, Vancouver V6T 1Z4, Canada. ³ School of Life Science and Biotechnology, Dalian University of Technology, Dalian, Liaoning 116023, China. ⁴ Department of Bioinformatics and Biotechnology, Government College University Faisalabad, Faisalabad 38000, Pakistan.

Acknowledgements

We appreciate the kind support of Prof. Feng-Wu Bai. We also would like to thank Xue-Mi Hao, Bo-Yu Geng, and Bo-Wen Jin for technical assistance and valuable discussion.

Competing interests

The authors declare that they have no competing interests.

Availability of data and materials

All data are presented in this main manuscript.

Consent for publication

Not applicable.

Ethics approval and consent to participate

Not applicable.

Funding

This work was supported by the National Natural Science Foundation of China [Grant Numbers 51561145014, 21536006, 21406030].

Publisher's Note

Springer Nature remains neutral with regard to jurisdictional claims in published maps and institutional affiliations.

Received: 7 September 2017 Accepted: 14 November 2017

Published online: 27 November 2017

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